

REPLACEMENT HAFNIUM CONTROL RODS FOR THE BONUS REACTOR 314

G. M. Tolson, G. R. Davis

Gerald M. Tolson (left) (BS, Purdue) is employed by Union Carbide Corporation, Nuclear Division, working at the Oak Ridge Gaseous Diffusion Plant where he heads the Reactor Components Group. His experience has been in the metallurgical engineering aspects of the design, construction, and operation of nuclear reactors and reactor tests. George R. Davis (BS, Pennsylvania State University) is vice president and marketing manager of Nuclear Components, Inc. He has been active in fabrication of control rods and other reactor internals since 1956.

DEPARTMENTS

CONTENTS	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	222
CORRIGENDA -	-	-	-	-	-	-	-	-	-	-	-	-		-	-	225
BOOK REVIEWS	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	321

Corrigenda

On November 25, 1969, W. E. Downs requested that we publish the following corrigendum that appeared in his article "Characteristics of a Continuous "On-Stream" Analysis System Using a Multikilocurie ¹²⁴Sb-Be Neutron Source" in the November issue.

Delete the following:

Page 468, Eq. (2), the term "g" which is not required when f_t is in g/cm^3 .

Downs states that all the data and conclusions are correct since the proper equation was used in all calculations.

On December 8, 1969, W. B. Lewis requested that we publish the following corrigenda that appeared in his

article "A Practical Approach to Nuclear Criticality Safety" in the December issue.

Correct the following:

Page 526, six lines from the bottom of column 2, which presently reads:

For RL,

$$J_1 = T_1^2 J_1^+, J_2^- + T_2^2 J_2^+$$

should read:

For RL,

$$J_{1}(u_{1}) = T_{1}J_{1}(-u_{1}), \ J_{2}(u_{1}) = T_{2}T_{2}(-u_{1})$$

Page 527, last line of second paragraph in column 2, which presently reads:

$$\omega_i = (1 - T_i^2 / (1 + T_i^2)),$$

should read:

$$\omega_j = (1 - T_j)/(1 + T_j)$$