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Effect of Temperature Variation on "Intermediate-Resonance" Formulas

The "intermediate-resonance" formulas derived by Goldstein and Cohen (1) for effective resonance integrals in homogeneous systems have found wide acceptance as a means of interpolating between the extreme "narrowresonance" and "infinite-mass" approximations at absolute zero temperature. However, there appears to be no reference in the literature to the validity of applying these formulas to the determination of effective resonance integrals at working temperatures. The effect of temperature variation is considered in this note.

Theoretical Background

Neglecting interference scattering and the variation in the reciprocal of the energy over a resonance, we may write the first and second order approximations to the effective resonance integral at working temperatures in the form

$$
I_{\lambda}^{(1)} = \frac{\Gamma_{\gamma} \sigma_0 a_{\lambda}}{2E_0} \int_{-\infty}^{\infty} \frac{\psi(\theta, x)}{a_{\lambda} + \psi(\theta, x)} dx \qquad (1)
$$

and

$$
I_{\lambda}^{(2)} = I_1^{(1)} \left[\frac{1 + \sigma_{pa}(1 - \alpha)}{\alpha \sigma_p} \right] + \frac{\Gamma_{\gamma} \sigma_{pa}(a_{\lambda} - a_{\infty})}{2E_0 x_0 a_{\infty}}
$$

$$
\cdot \int_{-\infty}^{\infty} \frac{\psi(\theta, x)}{a_1 + \psi(\theta, x)} \int_{x}^{\frac{x + x_0}{\alpha}} \frac{\psi(\theta, x')}{a_{\lambda} + \psi(\theta, x')} dx' dx,
$$
 (2)

where the notation is the same as that used by Dresner (2) , except that

$$
a_{\lambda} = \Gamma(\sigma_m + \lambda \sigma_{pa})/\sigma_0(\Gamma_{\gamma} + \lambda \Gamma_n),
$$

\n
$$
a_1 = \sigma_p/\sigma_0 = \text{Dresner's }\beta,
$$

\n
$$
a_{\infty} = \Gamma \sigma_{pa}/\Gamma_n \sigma_0
$$

and

$$
x_0 = 2E_0(1-\alpha)/\Gamma.
$$

Equations (1) and (2) give, to first and second order respectively, the "infinite-mass" approximation if λ is put equal to zero and the "narrow-resonance" approximation if λ is taken as unity. These extreme approximations may be combined linearly, following Goldstein and Cohen (1), to give

$$
I_{\mu}^{(1)} = (I_0^{(1)} + \mu I_1^{(1)})/(1 + \mu)
$$
 (3)

and

$$
I_{\mu}^{(2)} = (I_0^{(2)} + \mu I_1^{(2)})/(1 + \mu), \tag{4}
$$

where the "best" value of I results from the choice of μ in

such a way that
$$
I_{\mu}^{(1)} = I_{\mu}^{(2)}
$$
. Hence
\n
$$
\mu = (I_0^{(1)} - I_0^{(2)})/(I_1^{(2)} - I_1^{(1)})
$$
\n
$$
a_0 J(\theta, a_0) - a_1 J(\theta, a_1) \left[\frac{1 + \sigma_{pa}(1 - \alpha)}{\alpha \sigma_p} \right]
$$
\n
$$
- \frac{a_1 \sigma_{pa}(a_0 - a_x)}{2a_x \sigma_p x_0} L(\theta, a_1, a_0, x_0)
$$
\n
$$
= \frac{a_1 J(\theta, a_1) \sigma_{pa} \frac{(1 - \alpha)}{\alpha \sigma_p} + \frac{a_1 \sigma_{pa}(a_1 - a_x)}{2a_x \sigma_p x_0} L(\theta, a_1, a_1, x_0)}
$$
\n(5)

where

$$
L(\theta, a_1, a_\lambda, x_0) = \int_{-\infty}^{\infty} \frac{\psi(\theta, x)}{a_1 + \psi(\theta, x)} \cdot \int_{x}^{(x+x_0)/\alpha} \frac{\psi(\theta, x')}{a_\lambda + \psi(\theta, x')} dx' dx
$$

and $J(\theta, a_{\lambda})$ is the well-known function tabulated by Dresner *(2)* and others.

Equation **(5)** may be used to give an interpolation parameter, μ , appropriate for use in (3) or (4) at any given temperature .

Numerical Procedure

(i) Generation of $\psi(\theta, x)$

The line shape function was obtained by solving the differential equation

$$
\psi''(\theta, x) = \frac{1}{4}\theta^4 - \theta^2 x \psi'(\theta, x) - \frac{1}{4}\theta^2 (2 + \theta^2 + \theta^2 x^2) \psi(\theta, x), \quad (6)
$$

where the primes denote differentiation with respect to the variable x . The infinite range required for the integrals was truncated to the range $x = -d$ to $x = d$, and the range subdivided into *2j* equal steps in *x* of width *h.* It was necessary to choose d so that x_0/h was exactly an even integer *n.*

Using the notation

$$
x_i = -d + (i-1)h
$$

and

$$
\psi_i = \psi(\theta, x_i),
$$

the line shape function was obtained from the following algorithm.

$$
i = j + 1 \text{ (center of resonance)}:
$$
\n
$$
\psi_i = \frac{1}{2} \sqrt{\pi} \theta e^{\theta^2/4} \text{ erfc } \frac{1}{2} \theta,
$$
\n
$$
\psi_i' = 0.
$$
\n(7)

 $2j + 1 + n \ge i > j + 1$ and $x_i < 12/\theta$:

$$
\psi_i = \psi_{i-1} + h\psi'_{i-1} + \frac{1}{2}h^2\psi''_{i-1} + \frac{1}{6}h^3\psi'''_{i-1},
$$

\n
$$
\psi_i' = \psi'_{i-1} + h\psi''_{i-1} + \frac{1}{2}h^2\psi'''_{i-1}
$$

\n
$$
\psi''_i = \frac{1}{4}\theta^4 - \theta^2x_i\psi_i' - \frac{1}{4}\theta^2(2 + \theta^2 + \theta^2x_i^2)\psi_i,
$$

\n
$$
\psi'''_i = -\theta^2x_i\psi''_i - \frac{1}{4}\theta^2(6 + \theta^2 + \theta^2x_i^2)\psi_i' - \frac{1}{2}\theta^4x_i\psi_i.
$$

 $2j+1+n\geq i>j+1$ and $x_i\geq 12/\theta$: $\psi_i = \frac{1}{1+x_i^2} \left\{ 1 + \frac{2(3x_i^2-1)}{\theta^2(1+x_i^2)^2} \right\}$ $1 \leq i < j + 1$:

$$
\psi_i = \psi_{2j+2-i} .
$$

(ii) Evaluation of $J(\theta, a_{\lambda})$

The Doppler broadening function was evaluated using Simpson's rule, with a correction for the truncated range based on the assumption that $\psi = (1 + x^2)^{-1}$ in the wings of the resonance.

$$
J(\theta, a) = h \sum_{i=1}^{j+1} S_i r_i^{(\lambda)} + \frac{1}{a_{\lambda} c_{\lambda}} \left(\frac{\pi}{2} - \tan^{-1} \frac{d}{c_{\lambda}} \right), \quad (8)
$$

where

$$
\langle S_i \rangle = \frac{1}{3} (1, 4, 2, 4, \cdots, 2, 4, 1),
$$

$$
c_{\lambda} = \left(1 + \frac{1}{a_{\lambda}} \right)^{1/2}
$$

and

$$
r_i^{(\lambda)} = \frac{\psi_i}{a_\lambda + \psi_i}.
$$

(iii) Evaluation of $L(\theta, a_1, a_\lambda, x_0)$

To facilitate the calculation of the L-function, α was set equal to unity in the limit of integration. The effect of this simplification is negligible. Simpson's rule was again used and an end correction was added assuming $\psi = (1 + x^2)^{-1}$.

$$
L(\theta, a_1, a_\lambda, x_0) = h^2 \sum_{i=1}^{2j+1} S_i r_i^{(1)} q_i^{(\lambda)}
$$

+
$$
\frac{1}{a_1 a_\lambda (x_0^2 + c_\lambda^2)} \left[\ln \left(\frac{d + x_0}{d - x_0} \right) - \frac{2x_0}{c_\lambda} \left(\frac{\pi}{2} - \tan^{-1} \frac{d}{c_\lambda} \right) \right],
$$
 (9)

where

$$
q_i^{(\lambda)} = \sum_{k=i}^{i+n} S_k r_k^{(\lambda)}
$$

= $q_{i-1}^{(\lambda)} + \frac{1}{24} \{9(r_{i+n}^{(\lambda)} - r_{i-1}^{(\lambda)}) + 19(r_{i+n-1}^{(\lambda)} - r_i^{(\lambda)})$
= $5(r_n^{(\lambda)}) - r_{i-1}^{(\lambda)}) + (r_{i-1}^{(\lambda)} - r_{i-1}^{(\lambda)})$ (10)

- 5(ra U - n!X ⁺i) + (r£L , - rfti)}- E_{exact} on E_{time} subject the first step ϵ the first step and is step and is not all except step and is not at the first step and is not at the first step and is not at the magnetic step and is not at the magnetic $b = i \text{ and } b = i + n$ $k = i$ and $k = i + n$.

(iv) Order of Accuracy

The values found to be suitable for the numerical parameters were $h = 0.25$ and $d = 120$. Using these parameters, ψ was checked against the tabulation of Rose *et al.* (3) and found to differ on spot checks by at most 2% . The J -function was similarly checked against the accurate table values of Bell *et al.* (4) and the greatest error found was 0.1%. The *L-*function was checked in the limits

$$
\theta \to \infty
$$
 and $x_0 \to \infty$

and was found in each case to differ from the analytic result by less than $\frac{1}{2}\%$. (See Eq. (11).)

The numerical procedure was coded in FORTRAN for an I BM 1620 computer and each run took approximately 25 min.

Discussion of Results

Values of μ and I_{μ} have been determined from Eqs. (5) and (3) for several resonances of U²³⁸ in a homogeneous 1:1

TABLE I **COMPARISON OF RESONANCE INTEGRALS FOR** U^{238} **:** $H = 1:1$

E_0 (ev)	Temp. $({}^{\circ}{\rm K})$	μ	I_{μ} (barns)	$I_{\mu(0)}$ (barns)
6.68	$\mathbf{0}$	0.0510	4.06	4.06
	300	0.0496	4.10	4.10
	600	0.0485	4.15	4.15
	900	0.0476	4.20	4.20
21	0	0.262	1.80	1.80
	300	0.252	1.83	1.83
	600	0.244	1.87	1.87
	900	0.237	1.90	1.90
36.8	0	0.0189	1.46	1.46
	300	0.0204	1.49	1.49
	600	0.0220	1.51	1.51
	900	0.0234	1.53	1.53
66.3	$\bf{0}$	0.337	0.492	0.492
	300	0.359	0.522	0.523
	600	0.348	0.553	0.553
	900	0.325	0.581	0.581
$103\,$	0	0.554	0.402	0.402
	300	0.583	0.415	0.418
	600	0.593	0.430	0.433
	900	0.588	0.445	0.448
117	0	1.28	0.182	0.182
	300	1.38	0.221	0.222
	600	1.23	0.252	0.252
	900	1.06	0.278	0.277
192	0	1.57	0.172	0.172
	300	1.68	0.178	0.180
	600	1.74	0.184	0.188
	900	1.74	0.191	0.195
209	0	3.01	0.107	0.107
	300	3.32	0.121	0.122
	600	3.16	0.134	0.135
	900	2.93	0.146	0.146

mixture with hydrogen at temperatures ranging from $0^{\circ}K$ to 900°K. These values are recorded in Table I together with corresponding values of $I_{\mu(0)}$, which result from interpolation between the "infinite-mass" and "narrow-resonance" approximations at the specified temperatures using the appropriate 0° K value of μ .

The results show that, for a 1:1 mixture of U²³⁸ and hydrogen, there is virtually no difference between $I_{\mu(0)}$ and I_{μ} for most of the resonances considered, the maximum variation being about 2% for the 192 ev resonance.

In the case of the 192 ev resonance, the calculations were carried out for mixtures of U²³⁸ with hydrogen of various dilutions ranging up to 1:100, and the results are recorded in Table II. It appears that the difference between $I_{\mu(0)}$ and I_{μ} does not become significant except in very dilute mixtures, when the resonance escape probability is not very sensitive to changes in the effective resonance integral.

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TABLE					
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Comparison of Resonanc e Integrals fo r th e 192 ev **Resonanc e of U²³⁸**

As expected, the trend in the interpolation parameter with increasing dilution is towards the "narrow-resonance" limit. Another trend which becomes apparent from a consideration of dilute mixtures is that μ moves back towards the "infinite-mass" value as the temperature increases.

The results as a whole show that, although the interpolation parameter μ may exhibit quite marked changes with temperature in some cases, the variation has a comparatively small effect on the effective resonance integral. Thus it appears that, in applying the formulas of Goldstein and Cohen, no significant error should result from the use of the 0° K value of μ in the calculation of the total effective resonance integral, except, perhaps, when determining the Doppler coefficient, for which a more thorough investigation may be needed.

It is interesting to note that, for the values of the parameters relevant to the resonances of Th²³² and U²³⁸ under practical conditions, the function $L(\theta, a_1, a_\lambda, x_0)$ has been found to be given within a few percent by the formula

$$
L(\theta, a_1, a_\lambda, x_0) \simeq \frac{4}{\pi} J(\theta, a_1) J(\theta, a_\lambda) \tan^{-1} \frac{x_0}{c_1 + c_\lambda}, \quad (11)
$$

which is exact in the limit as $\theta \rightarrow \infty$ and also in the limit as $x_0 \rightarrow \infty$.

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The Average Capture/Fission Ratio of U²³³ for Epithermal Neutrons

In thermal reactors using U²³³ as fuel somewhere around 10% of all absorption in the fuel may be expected to involve epithermal neutrons. While the capture/fission ratio α for thermal neutrons is known to be close to 0.10 (I) and while the fission, scattering, and total (i.e., fission plus capture plus scattering) cross sections have been studied as a function of energy (1) , nevertheless there remains significant uncertainty as to the average capture cross section and capture/fission ratio for epithermal neutrons. If the latter ratio were sufficiently high the consequent effect on the neutron economy of a U^{233} thermal breeder could be serious. The purpose of the work described here was to to compare the epithermal capture and fission values to the thermal values by the use of Cd ratios, radiochemical analyses of fission products, and mass-spectrographic ratios of U²³⁴/U²³³. Thereby an experimental α_{epi} for epithermal neutrons was evaluated, as were infinitely dilute resonance integrals for capture and fission, I_c and I_f , for U²³³.

Microgram quantities of **U²³³** (prepared to be especially free of **U²³⁴** by milking **U²³³** from Pa²³³) were irradiated in both the LITR (ORNL Low Intensity Test Reactor) and ORR (Oak Ridge Research Reactor), both with and without 40 mil Cd filters surrounding them. The thermal fluxes were about 2×10^{13} and 1×10^{14} n/cm²-sec respectively. Both thermal and epithermal fluxes were monitored at the sample positions with cobalt in a dilute Co-Al alloy (containing 0.151% Co).

After irradiation, the uranium was separated from fission products and other impurities and analyzed mass-spectrographically for **U²³⁴** produced. Analyses were made on the four fission products, 12.8 -day Ba¹⁴⁰, 67 -hr Mo⁹⁹, 54 -day Sr⁸⁹ and 65-day Zr⁹⁵, by using standard procedures (2) with few modifications, in order to determine the number of fissions which occurred during irradiation. ¹

¹The yield of I¹³¹ was also measured and found to give a resonance integral some 36% higher than that computed from Sr⁸⁹, Mo⁹⁹, and Ba¹⁴⁰. Since I¹³¹ is on the slope of the