LETTERS TO THE EDITORS

## Space-Time Burnout of an Absorbing Slab

Consider a nonscattering absorbing slab extending from x = 0 to x = D. Assume a constant current of neutrons of strength  $\phi_0$  entering at x = 0 normal to the surface, and starting at time zero. Let the slab have a single absorbing species of microscopic cross section  $\sigma$  barns and initial number density  $N_0$  nuclei per barn-cm. Then, at any time t and depth x, the neutron current and absorber number density satisfy the following simultaneous integral equations:

$$N(x, t) = N_0 \exp\left[-\sigma \int_0^t \phi(x, t') dt'\right]$$
(1)

$$\boldsymbol{\phi}(x,t) = \boldsymbol{\phi}_0 \exp\left[-\sigma \int_0^x N(x',t) \, dx'\right]. \tag{2}$$

These equations can easily be transformed to a pair of simultaneous differential equations by changing to a new set of variables:

$$u(x) = \sigma nvt \text{ at depth } x = \sigma \int_0^t \phi(x, t') dt' \qquad (3)$$

v(t) =depth in mean free paths

$$= \sigma \int_0^x N(x', t) \, dx'. \tag{4}$$

Equations (1) and (2) become

$$\partial v / \partial x = \sigma N_0 e^{-u}$$
 (5)

$$\partial u/\partial t = \sigma \phi_0 e^{-v}. \tag{6}$$

A solution is easily found in the following form<sup>1</sup>

$$u = \ln \left[ 1 + e^{\sigma \phi_0 t - \sigma N_0 x} - e^{-\sigma N_0 x} \right]$$
(7)

$$v = \ln \left[ 1 + e^{\sigma N_0 x - \sigma \phi_0 t} - e^{-\sigma \phi_0 t} \right].$$
(8)

The  $\phi$  and N can be obtained by differentiation but often u and v are themselves more valuable. For example, v(D) is the mean free path depth of the slab at any time.

A similar case of greater interest is simply to solve the same problem when the slab is subjected to a normally incident current from both sides. In this case let the total thickness of the slab be 2x, and examine the conditions which apply at the center

$$\boldsymbol{\phi}(x, t) = 2\boldsymbol{\phi}_0 \exp\left[-\sigma \int_0^x N(x', t) \ dx'\right] \tag{9}$$

<sup>1</sup> This solution proceeds from the fact that  $\partial^2 u/(\partial x \partial t)$ and  $\partial^2 v/(\partial x \partial t)$  are equal, so that u + h(x) = v + g(t). The solution follows upon insertion into Eqs. (5) and (6) and use of boundary conditions.

$$N(x, t) = N_0 \exp\left[-\sigma \int_0^t \phi(x, t') dt'\right].$$
 (10)

The solution proceeds in the same manner as above, yielding the following value for the slab depth (in mean free paths) as a function of time:

$$2v(x, t) = 2 \ln \left[1 + e^{N_0 \sigma x - 2\phi_0 \sigma t} - e^{-2\phi_0 \sigma t}\right].$$

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## Concerning the Theory of Control Sheets

In a recent paper (1), Wolfe derived a critical condition for a plane symmetric reactor with plane control sheets inserted, under the conditions that

$$\delta \gg \min(L, \sqrt{\tau})$$
 (1)

where  $\delta$  is the spacing between sheets, and L,  $\tau$  are the thermal diffusion length and age in the core material. In particular, a critical equation of the form

$$(\sin \mu \delta, \cos \mu \delta)(\alpha \lambda_1^N V_1 + \beta \lambda_2^N V_2) = 0$$
(2)

has been given for N equally spaced sheets, where  $\alpha$ ,  $\beta$ ,  $\lambda_1$ ,  $\lambda_2$  are functions of the material properties, and  $V_1$ ,  $V_2$  are vector functions of these properties.

Equation (2) was derived from the condition

$$(\sin \mu \delta, \cos \mu \delta) Q^N \begin{pmatrix} 1 \\ 0 \end{pmatrix} = 0$$
 (3)

where

$$Q = \begin{pmatrix} \cos \mu \delta + R \sin \mu \delta & -\sin \mu \delta + R \cos \mu \delta \\ \sin \mu \delta & \cos \mu \delta \end{pmatrix}$$
(4)

and R is a function of material properties.

In the following we will show how the critical equation, Eq. (2), can be considerably simplified by working from Eqs. (3) and (4) in a somewhat different manner than was done in ref. 1.

It was shown in ref. 1 that the eigenvectors  $V_1$ ,  $V_2$  of

Q are

$$V_1 = \begin{pmatrix} S - RC\\ RS/2 - \sqrt{T^2 - 1} \end{pmatrix}$$
(5)