## **Modification to Prescription for**  *[kfi/Jt]* **Pulsing**

**Pulsed neutron generators used in reactor research can be grouped into two general classes: sealed-off tube devices in which the target potential is pulsed; and accelerator systems in which the target is operated dc, and pulsing is derived by electrostatic deflection of the ion beam. In the event of the latter, a certain amount of leakage beam is invariably present between pulses. This leakage beam, although measuring only 10"2 to 10""<sup>4</sup> times the pulsed current, can constitute a source of comparable magnitude to the low-duty factor pulses.** 

**When the derivation of Garelis and Russell1 is repeated with the addition of a steady-source term, Eq. (27) becomes** 

$$
N_n = e^{-\alpha_n \tau} + \frac{R}{\alpha_n \hat{\mathfrak{F}}_n} + \frac{Q\ell}{\Delta k_n},
$$
 (1)

**where the source strength'Q' represents the effect**  of the leakage beam and of any  $(\alpha,n)$ ,  $(\gamma,n)$ , or **spontaneous fission reactions taking place in the**  assembly. In contrast to the conventional  $\alpha'$  technique, the  $(k\beta/\ell)$  method requires a determination **of the fraction of the between-pulse flux which is produced by the steady-neutron sources. Ordinarily, this presents only a simple background-subtraction problem2. However, in the case of the accelerator neutron generators, the situation is slightly more complicated, and the prescription given by Garelis3 must be modified as follows:** 

**After tuning up the accelerator, deflect the beam off, and wait until equilibrium is established. Start recording with the first pulse, and continue until adequate counting statistics are obtained. Then, with the accelerator otherwise still functioning, deflect the beam off, and continue counting for a time that is long compared to the longest-lived precursor. Finally, with no change in the accelerator settings, determine the effect of steady sources by starting a new measurement comprising an equal number of sweeps.** 

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## **Empirical Gamma-Ra y Albed o Formula\***

**Differential dose albedo measurements have been made at the U. S. Naval Radiological Defense Laboratory (USNRDL) using Cs137 and Co80 as sources, 'semi-infinite' slab thicknesses of concrete, iron and aluminum as scattering media and three angles of incidence. More than 300 measured values of dose albedo were collected using a plastic scintillator as the transducer of a pulsedosimetry system having a reproducibility of better than 1% and an estimated probable error on the order of 5%.** 

**Since differential dose albedo measurements are used as input data for engineering shielding calculations it is desirable that they be convertible**  into analytic form. To this end, differential dose albedo data points,  $\alpha_d$ , for a particular source energy,  $E_0$ , angle of incidence,  $\theta_0$ , and slab ma**energy,** *E0,* **angle of incidence,** *60,* **and slab material, Z, were converted** to  $A_d = \{a_d \mod 2 \}$  and **plotted versus the Compton scattering angle,**  $\theta_s$ **, in radians. It was found that each set of plotted points could be represented by an empirical for**mula,  $A_d$ (emp) =  $c e^{-m\theta_s} + b'$ , where each of the **adjustable parameters c,** *m,* **and** *b<sup>r</sup>*  **is a function of**   $E_0$ ,  $\theta_0$ , and *Z*. The deviations of the empirical  $A_d$ 's **from the experimental were on the order of 3%.** 

**Further, it was found that if suitable average**  values  $\bar{c}$  and  $\bar{m}$  were selected, all of the dose al**bedo data points taken\_could be fit by a single formula,**  $A_d$ (emp) =  $\overline{c}e^{-\overline{m}\theta_s} + b$ , where now only *b* is **a** function of  $E_0$ ,  $\theta_0$ , and Z. This simplification is **necessarily accompanied by some loss of accuracy.** 

In the figure, the differences,  $A_d - b$ , between the **measured dose albedo values and the fitting parameter** *b,* **are plotted as points and the function**   $e^{-\pi\theta_s}$  is drawn as a solid curve. The empirically determined values of *b* for each( $E_0$ , $\theta_0$ , $Z$ ) configur**ation are tabulated in the figure. The selection of 1** for  $\overline{c}$  and  $\pi$  for  $\overline{m}$  was made by an approximation **process. No fundamental significance is to be inferred from their presence in the formula since they were chosen partly for their mnemonic value.** 

**Although no extensive effort was made to opti**mize the fit,  $90\%$  of the data points,  $A_d$ , fall within 15% of the value,  $A_d$  (emp), predicted by the formula for the same angle,  $\theta_s$ .

**<sup>X</sup>E. GARELIS and J. L. RUSSELL, Jr.,** *NucL Sci. Eng.,*  **16, 263 (1963).** 

**<sup>2</sup>P. MEYER,** *Trans. Am. NucL Soc.,* **6, 287 (1963). <sup>3</sup>E. GARELIS,** *Nucl. Sci. Eng.,* **18, 242 (1964).** 

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**lD. J. RASO, "Monte Carlo Calculations on the Reflection and Transmission of Scattered Gamma Rays,"** *Nucl. Sci. Eng.* **17, pp. 411-418 (1963).** 

<sup>&</sup>lt;sup>2</sup>A. B. CHILTON and C. M. HUDDLESTON, "A Semi-**Empirical Formula for Differential Dose Albedo for Gamma Rays on Concrete."** *NucL Sci. Eng.* **17, pp. 419-424 (1963).**