For an average slip ratio <3.109, $\rho_l - 2\bar{\rho}$ is positive, so increasing slip increases the circulation ratio. Since the conditions assumed here are similar to those from Ref. 1 cited above, the behavior reported there is physically reasonable.

quently used operators is available in handbooks (see Ref. 4). Let us assume Eq. (2) to have a unique solution that is sufficiently smooth.³ The solution of Eq. (2) then has the following form:

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REFERENCES

I. G. W. HOPKINS, A. Y. LEE, and 0. J. MENDLER, "Thermal and Hydraulic Code Verification: ATHOS2 and Model Boiler No.2 Data," Vol. I, EPRI NP-2887, Electric Power Research Institute (Feb. 1983).

2. G. S. LELLOUCHE and B. A. ZOLOTAR, "A Mechanistic Model for Predicting Two-Phase Void Fraction for Water in Vertical Tubes, Channels and Rod Bundles," EPRI NP-2246-SR, Electric Power Research Institute (1982).

3. L. W. KEETON et a!., "The URSULA2 Computer Program, Vol. 2: Applications (Sensitivity Studies and Demonstration Calculations)," EPRI NP-1315, Electric Power Research Institute (Jan. 1983). Used by permission.

Richardson Extrapolation

The only aim of the present Letter is to draw the readers' attention to an old method¹ for increasing the accuracy of numerical solutions of linear problems. Customarily, new finite element (FE) or coarse-mesh (CM) algorithms are checked on well-defined benchmark problems,² and the reference solution of a given benchmark problem is usually obtained by a wellestablished program using a large number of meshes.

We are concerned here with the Richardson extrapolation,³ which allows one to obtain higher accuracy without refining further the mesh. The method can be used independently of the geometry.

It is well known that the accuracy of a numerical solution is often proportional to some power of the mesh size h . The accuracy of the finite difference (FD) method is $O(h)$, that of the linear FE method is $O(h^2)$. The basic idea in Richardson extrapolation is to separate a part of the error, proportional to some power of h , and to eliminate it. Let us consider the problem to be solved as

$$
Lu = f \quad \text{in} \quad \Omega \tag{1a}
$$

$$
Bu = g \quad \text{on} \quad \partial \Omega \tag{1b}
$$

where $\partial\Omega$ is the boundary of the region Ω . In numerical methods Eq. (1) is substituted by the discretized formulas

$$
L_h u_h = f_h \quad \text{in} \quad \Omega_h \tag{2a}
$$

$$
B_h u_h = g_h \quad \text{on} \quad \partial \Omega_h \tag{2b}
$$

In the discretized formulas the dependence on the mesh size *h* is indicated explicitly. The discretized form of the most fre-

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Richardson Extrapolation of BUG-180 Results, Using 3 and 12 Points per Hexagon, Problem GA9A1

^aBn: BUG-180 result using *n* points per hexagon.

^bRE: Richardson extrapolation.

cUNIV AC 1108 CPU min.

$$
u_h = u + \sum_{j=1}^{m} v_j h^j + \eta_h , \qquad (3)
$$

where

- $u =$ exact solution of Eq. (1)
- h = mesh size
- v_i = functions independent of *h*
- η_h = so-called remainder
- $m =$ integer connected with the smoothness⁵ of functions f and g .

Let us form a linear expression from the approximate solutions u_{h_k} associated with mesh size h_k as follows:

$$
V = \sum_{k=1}^{m+1} \gamma_k u_{h_k} \tag{4}
$$

and the weighting γ_k is obtained from

$$
\sum_{k=1}^{m+1} \gamma_k = 1 \tag{5}
$$

$$
\sum_{k=1}^{m+1} \gamma_k \cdot (h_k)^j = 0 \, , \quad j = 1, \dots, m \, . \tag{6}
$$

For example, if $h_1 = H$ and $h_2 = H/2$ then $\gamma_1 = -1/3$; γ_2 = 4/3. The following estimation is valid for V:

$$
V - u = \sum_{k=1}^{m+1} \gamma_k \cdot \eta_{h_k} \tag{7}
$$

Let us remark that the error of *V* does not include any part proportional to some power of the mesh size. An estimation of the functions η_{h_k} is available through the smoothness of the coefficients figuring in the original operator *L.* To take an example, in the one group diffusion equation, let the coefficients belong^a to $C'[0,1]$, in which case the estimation

$$
|V - u| \leq c \cdot h^r \tag{8}
$$

holds. Usually $r > 2$ so the error of the approximate solution V is smaller than the error of any u_{h_k} .

To illustrate the method let us consider a high-temperature gas-cooled reactor benchmark² identified as GA9A1. In Table I

the FD solutions by the code BUG-180 using 3 and 12 points per hexagon and the Richardson extrapolated solution are compared with the solution using 48 points per hexagon. The applied weightings are

$$
V = -\frac{1}{3} u_h + \frac{4}{3} u_{h/2} , \qquad (9)
$$

where $h = 20.9$ cm. As we can see, the Richardson extrapolation has improved the accuracy considerably. It is pointed out that from a VENTURE-like⁶ FD solution one can obtain a solution in \sim 1 min [IBM 360/195 central processing unit (CPU)] that is not inferior in accuracy to CM or FE solutions. The author is convinced that opinions⁷ regarding the outstanding efficiency of CM and FE methods over FD methods should be revised.

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REFERENCES

I. L. F. RICHARDSON, *Philos. Trans. Roy. Soc., London, Ser.* A., 210, 307 (1910).

2. *Benchmark Problem Book,* ANL-7416, Suppl. 2, Argonne National Laboratory (1977).

3. G. I. MARCHUK and V. V. SHAIDUROV, *Difference Methods and Their Extrapolations,* Springer Verlag, New York (1983).

4. G. A. KORN and T. M. KORN, *Mathematical Handbook for Scientists and Engineers,* McGraw-Hill Book Company, New York (1970).

5. For further details see Ref. 3, p. 16.

6. D. R. VONDY and T. B. FOWLER, "VENTURE," ORNL-5062, Oak Ridge National Laboratory (1975).

7. R. D. LAWRENCE and J. J. DORNING, *Nucl. Sci. Eng.,* 77, 502 (1981), express this rather general opinion; as evidence that the present author was of a similar opinion, see M. MAKAI and C. MAEDER, *Nucl. Sci. Eng.,* 84, 390 (1983).

 ${}^aC'[0,1]$ denotes the set of functions which are *r* times continuously differentiable on [0,1].